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Article

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Research Paper

Optimal Designing and Synthesis of a Hybrid PV/Fuel cell/Wind System using Meta-heuristics

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ABSTRACT

In this paper, a multi-objective optimization method has been established on a hybrid PV, wind, fuel cell, and battery system. The optimization is based on three models including energy supply reliability, electricity efficiency, and capital cost of the hybrid system. A new model of the Elephant Herding Optimization (BEHO) Algorithm is utilized to solve the multi-objective optimization problem and is validated based on different algorithms and benchmark functions. The main purpose is to determine the Pareto surface including a set of possible design solutions to help the decision-makers obtaining the global optimum solution. The final results indicated that the proposed method is an applicable approach for designing of the proposed hybrid system.

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1. Introduction

The world's orientation toward energy and moving toward an oil-free economy on the one hand and the various advantages of renewable energies, on the other hand, make it imperative to prioritize the development of these clean energies with various economic and environmental benefits (Liu et al., 2020). Improving citizens' awareness of the benefits of using renewable energies will certainly facilitate the development of cleaner energy in the world (Fathi et al., 2020). Special capacity for economic development, promotion of energy supply and security and environmental protection and reduction of air pollution are three important advantages of renewable energies. Also, the need to diversify the country's energy basket to improve energy security is another reason for the need to develop renewable energies. This is one of the priorities of the energy sector in light of the dramatic increase in energy demand in the coming years (Kiran and Chandrakala, 2020).

The scarcity of power grids in remote areas and the high cost of connecting these areas to national electricity networks lead to the use of other energy sources independently of the grid. One of the major problems with the use of renewable sources is the severity of the winds during the day and the lack of solar energy at night, which combines wind and solar systems (Fathi

et al., 2020; Aghajani and Ghadimi, 2018). These hybrid systems also have some problems such as low system reliability and lack of peak load during the year. To resolve this problem, different solutions can be proposed (Liu et al., 2017; Gollou and Ghadimi, 2017). One of the useful, new, and widely used method is to adopt fuel cells as the storage system of these systems. Several works have been performed in this orientation. For example, Mirzapour et al. (2019) presented and optimized a hybrid system based on fuel cell, biomass gasifier generator set, power conditioning unit, and battery backup for an academic section in Maulana Azad National Institute of Technology in India. The HOMER simulator was adopted for designing the grid and it simulated the financial criteria of the system (Hosseini Firouz and Ghadimi, 2016; Hamian et al., 2018; Leng et al., 2018; Akbary et al., 2019; Ebrahimian et al., 2018). The examination was executed in different conditions. The simulation results showed that the cost of energy (COE) for the biomass gasifier generator set, solar PV, and fuel cell crossover energy system has is about 15 Rs/kWh and complete net present cost (NPC) is 52 Rs/kWh.

Khodaei et al. (2018) proposed an optimized techno-economic grid-connected hybrid system including wind, solar, and fuel cell for residential applications. The storage system was utilized for increased system reliability. Different parameters of the system were analyzed to achieve their effectiveness on the system. The Genetic Algorithm (GA) and the Particle Swarm Optimization algorithm were utilized for minimizing the system maintenance and operation cost. Final results showed the

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Nomenclature

A_s	Area of a single PV cell (m^2)
C_T	Tafel constant
E	Nernst Potential (v)
$f_{\text{maintenance}}$	Maintenance factor of SOFC
F	Faraday constant
i_{capital}	Capitalization ratio
I	Fuel cell stack current (A)
J	Current densities
N	Number of tubes
N_b	Lifespan of batteries (year)
N_p	Lifespan of project (year)
N_{units}	Production volume of SOFC
N	Number of cells
P	Pressure
R	Resistance (Ω)
R_c	Connections resistance
R_m	Membrane resistance
S	Membrane area (cm^2)
S_s	Salvage value of PV panels ($$/\text{m}^2$)
T	Temperature ($^\circ\text{C}$)
U	Hydrogen utilization factor
V	Voltage (v)

Greek letters

α	Thermal voltage timing completion factor (V)
α_b	Initial cost of batteries ($$/\text{m}^2$)
α_s	Initial cost of PV panels ($$/\text{m}^2$)
α_{OMs}	Yearly operation and maintenance cost for solar ($$/\text{m}^2 \text{ year}$)
β	Parametric coefficient
λ	Tunable parameter
γ	Interest rate
κ	Inflation rate
ν	Escalation rate
η	Efficiency
ξ	Pseudo-experimental parametric coefficients
Ω	Ohmic loss
τ	Solar radiation (W/m^2)

Subscripts

a	Activation
b	Battery
c	Capacitance
c	Concentration
CO_2	Oxygen concentration at the cathode/gas interface (mol cm^{-3})
CH_2	Hydrogen concentration at the anode membrane /gas interface (mol cm^{-3})
elec	Electrolyzer
FC	Fuel cell
G	Electrical energy that is generated by the PV

and power source (CHP).

[Bagal et al. \(2018\)](#) studied a hybrid PV-Wind-Fuel Cell system and then, they optimized it for electricity production for remote sites in the Colombian Caribbean region. For performance analysis of the studied system, its simulation was applied to the demand of 200 W by considering the wind speed and the solar radiation variations for every single day in different regions. A multi-objective optimization was implemented to the study for minimizing the Levelized CO₂ emission and energy cost.

[Gheydi et al. \(2016\)](#) proposed a three-part hybrid system based on the thermal solar system, wind turbine and, and fuel cell. The presented system allowed to maximize the yearly generated electricity based on the supplied power optimizing yearly. The method was then applied to a practical case study in Lebanon. The final results showed a secure achievement toward different renewable energy sources variations.

[Firouz and Ghadimi \(2016\)](#) proposed an adaptive multi-agent management system for a CHP system in micro-grid. The CHP system contained three parts: wind turbine, Fuel cell, and PV. The controller for the system was based on a fuzzy controller. The main objective was to design the load frequency controller (LFC) to control the frequency oscillation of the agents and to minimize the production cost of the overall system. The PSO algorithm was used to the optimal selection of the key parameters of the controller to adjust the system efficiency.

[Eslami et al. \(2019\)](#) investigated a combine CHP system including PV, wind, fuel cell, and battery for a nursing home in Istanbul. The study used HOMER software to characterize the optimal configuration of the hybrid system by considering the cost of energy and the total NPC. Simulation results showed the best configuration for the hybrid system.

Based on the literature, there is a lot of researches that worked on the optimal unit sizing of the hybrid solar-wind DG system. This study presents a new configuration by combining a high-temperature polymer electrolyte membrane fuel cell (PEMFC) system (including the electrolyzer and the fuel cell stacks) with the hybrid wind/PV system. The system presents a multi-objective optimization technique by considering the efficiency, energy reliability, and cost of the hybrid model.

2. Mathematical modeling of the overall system

The analyzed model in this study is a hybrid model including wind turbine, fuel cell, and solar system with electrolyzer and cell stacks (wind/solar/fuel cell) to use during a long time with storing the energy for the required times. In the operation process, the surplus electrical energy which is produced by PV and wind is adopted for producing hydrogen using electrolyzer. Afterward, the generated hydrogen is stored in hydrogen reservoir tanks. The hydrogen reservoir tanks are then employed to generate electricity by supplying fuel cell stacks. [Fig. 1](#) indicates an energy management technique for the proposed hybrid DG based on ([Saeedi et al., 2019](#)).

2.1. Model of the fuel cell stack

This research utilizes a proton exchange membrane fuel cell (PEMFC) in the system due to its several advantages such as its higher efficiency and simple working. The model of the PEMFC stack is based on a steady-state model. The water is assumed as the membrane electrolyte saturator that makes it be a function of temperature. [Fig. 2](#) shows a simple circuit model of a PEMFC.

Thereupon, the PEMFC current density depends on the geometric features, the reactants quantity, and the hydrogen utilization factor.

$$I_{\text{FC}} = \frac{2 \times n_{\text{H}_2, \text{in}} \times U_{\text{FC}}}{N_{\text{FC}} \times A_{\text{FC}}} \quad (1)$$

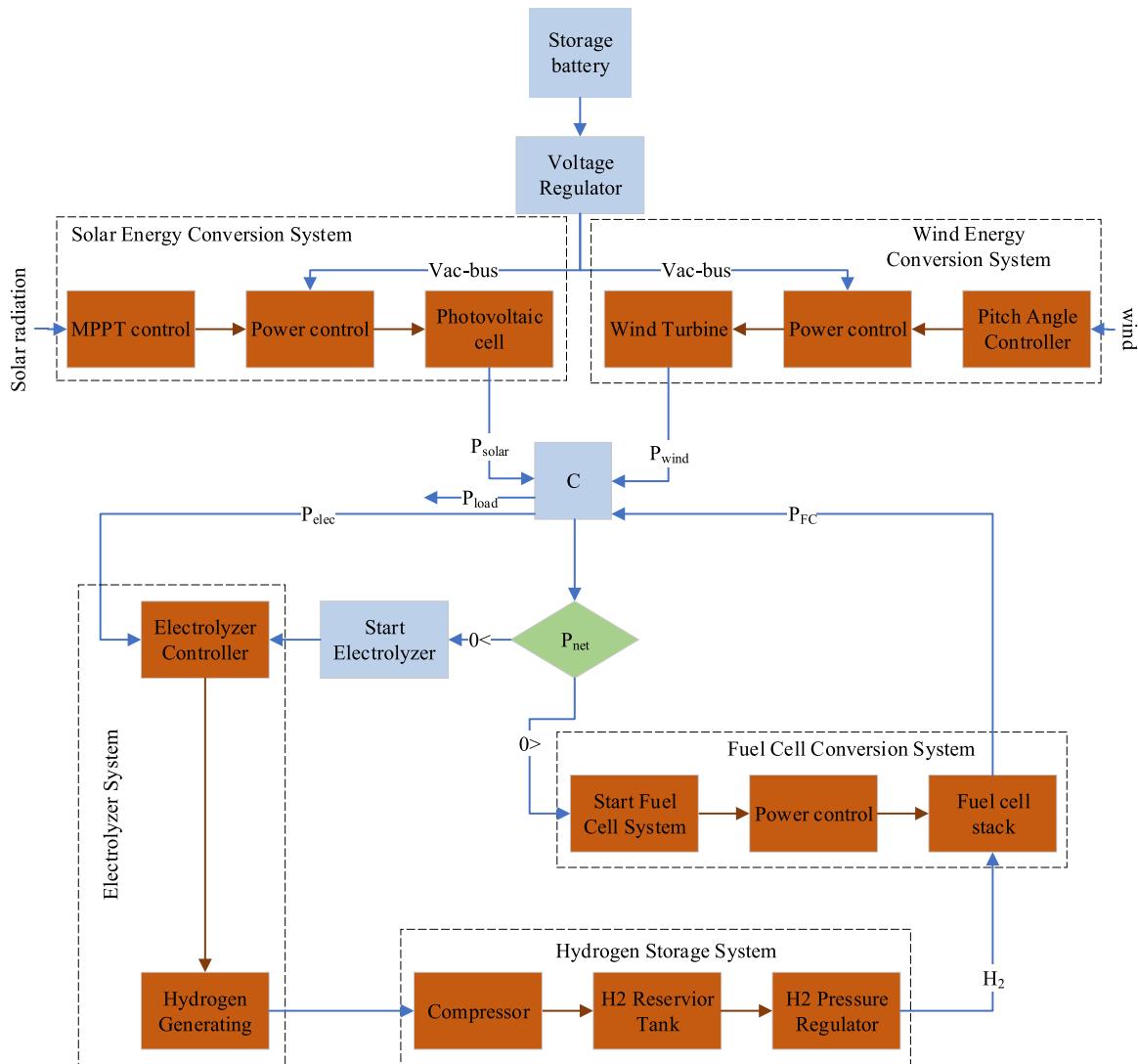


Fig. 1. The graphical conception of the energy management system for the presented hybrid system.

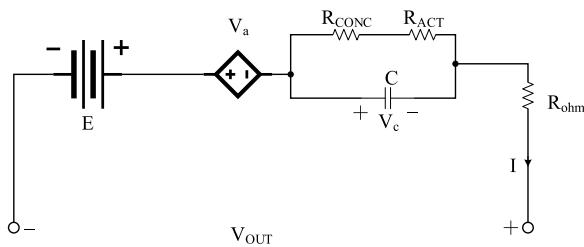


Fig. 2. The circuit model of a PEMFC.

where, $n_{H_2,in}$ stands for the number of H_2 tubes, U_{FC} describes the hydrogen utilization factor, N_{FC} is the cells number, and A_{FC} is the active area.

Following Fig. 2, the PEMFC output voltage is achieved can be achieved based on the following equation:

$$V_{OUT} = E - V_a - V_c - V_\Omega \quad (2)$$

where, V_a describes the activation loss voltage, V_c determines the concentration losses voltage, V_Ω stands for the ohmic losses voltage, and E describes the Nernst (reversible) potential and is

achieved as follows:

$$E = 1.23 + (-8.5 \times 10^{-4}) \times (T_{FC} - 298.15) + \frac{RT_{FC}}{4F} \ln \left(P_{H_2} \sqrt{P_{O_2}} \right) \quad (3)$$

The activation loss decreases the reactions speed on the electrode's surface and can be formulated by the following equation:

$$V_a = -0.95 + \times T + 7.6 \times 10^{-5} \times T \times \ln (CO_2) + 1.93 \times 10^{-4} \times T \times \ln (I_{FC}) \quad (4)$$

where, I_{FC} describes the PEM fuel cell stack current and CO_2 determines the oxygen concentration at the cathode/gas interface (mol cm^{-3}) by the following:

$$CO_2 = \frac{p_{O_2} \times e^{\left(\frac{498}{T}\right)}}{50.8 \times 10^7} \quad (5)$$

where, P_{O_2} stands for oxygen partial pressures (Pa).

And ξ describes the pseudo-empirical parametric and this (Re-strepo et al., 2014).

$$\xi = 0.003 + 0.0002 \ln (A) + 43 \times 10^{-6} \ln (C_{H_2}) \quad (6)$$

And CH_2 stands for the Hydrogen concentration at the anode membrane/gas interface (mol cm^{-3}) and is achieved as follows:

$$\text{CH}_2 = \frac{p_{\text{H}_2} \times e^{\left(\frac{-77}{T}\right)}}{10.9 \times 10^7} \quad (7)$$

where, p_{H_2} describe the hydrogen partial pressures (Pa).

The Ohmic voltage drop for the fuel cells is modeled by the following:

$$V_{\Omega} = I_{\text{PEM}}(R_m + R_c) \quad (8)$$

where,

$$R_m = \rho_m l S^{-1} \quad (9)$$

$$\rho_m = \frac{181.6 \times \left[0.062 \left(\frac{T_{\text{FC}}}{303} \right)^2 \left(\frac{I_{\text{FC}}}{S} \right)^{2.5} + 0.03 \left(\frac{I_{\text{FC}}}{S} \right) + 1 \right]}{\left[\lambda - 0.063 - 3 \left(\frac{I_{\text{FC}}}{S} \right) \right] \times e^{\frac{T_{\text{FC}}-30}{T_{\text{FC}}}}} \quad (10)$$

where, S stands for the membrane area (cm^2), I describes the membrane thickness, I_{FC} determines the PEMFC operating current, T_{FC} represents the operating cell temperature (K), λ determines a tunable parameter, R_c and R_m describe the connections resistance and membrane resistance, and ρ_m stands for the resistivity of the membrane.

Finally, the concentration overvoltage can be also obtained based on the following equations:

$$V_C = -\beta \times \ln \left(J_{\text{max}} - \frac{J}{J_{\text{max}}} \right) \quad (11)$$

where, β stands for the parametric coefficient, J and J_{max} describes the typical and the maximum current densities, respectively.

2.2. Model of electrolyzer

The model of the electrolyzer is performed by the following assumption:

In the electrolyzer model, the water vapor of the electrolytic cells in the anode and the cathode are fully saturated and incompressible. The value of the temperature and the pressure for the electrolytic cells in gas flow channels are considered constants. The liquid and the gas phases are assumed separable. The enthalpy of the water vapor has been assumed constant during the working temperature. The working temperature for the electrolytic cells is considered 100 °C. The required energy for water supply and hydrogen compressing has been neglected.

The system cannot receive the maximum value that is due to the parasitic current losses. By considering the Faraday Law, the experimental hydrogen rate is achieved by the following equation (Guo et al., 2017):

$$\eta_I = 96.5 \times e^{\left(\frac{0.09}{I_{\text{el}}} - \frac{75.5}{I_{\text{el}}^2} \right)} \quad (12)$$

where, η_I describes the current efficiency and I_{el} represents the electrolyzer current density (A/cm^2).

And the rate of hydrogen production (mol/s) is obtained as follows:

$$r_{hp} = \frac{\eta_I \times I_{\text{el}} \times N_{\text{el}}}{2 \times F} \quad (13)$$

where, N_{el} describes the number of electrolytic cells, I_{el} stands for the electrolyzer current (A), F determines the Faraday constant ($F = 96487 \text{ C/mol}$).

Based on the explained assumptions, the Nernst equation (E) is considered to evaluate the reversible potential of the electrolytic cells that are explained before. The electrolytic cells have some

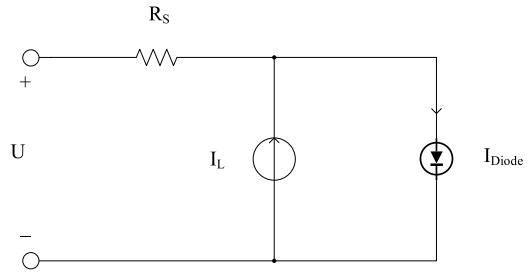


Fig. 3. The circuit model of a PV cell/module model.

unavoidable losses like ohmic, concentration polarization, and activation losses, the open-circuit voltage is greater than E . By neglecting the concentration overpotential loss due to its small value in electrolyzer cells (Yang et al., 2007), the open-circuit voltage can be formulated as follows:

$$V_{el} = E + V_{el}^{\Omega} + V_{el}^a \quad (14)$$

where, V_{el}^{Ω} describes the ohmic polarization loss for the cells (V), and V_{el}^a represents the activation polarization loss for the electrolytic cells (V) and is obtained by the following equation (Hoogers, 2002):

$$V_{el}^a = C_T + S_T l g i \quad (15)$$

where, $C_T = 0.06$ describes the Tafel constant, and $S_T = 0.1$ represents the Tafel slope.

Finally, the Ohmic Voltage loss is obtained as follows:

$$V_{el}^{\Omega} = 0.127 \times I_{el} \times e^{-2870 \times \left(\frac{1}{1273} - \frac{1}{T_{el}} \right)} \quad (16)$$

2.3. Model of PV cell/module

A simple circuit-based model of a PV cell can be determined by four parameters that are shown in Fig. 3. Based on Fig. 3, the load current can be achieved as follows (Chen et al., 2017).

$$I = I_L - I_D = I_L - I_0 \times \left[\exp \left(U + \frac{I \times R_s}{\alpha} - 1 \right) \right] \quad (17)$$

where U stands for the output voltage, I_0 represents the saturation current (A), R_s describes the series resistance (r), α describes the thermal voltage timing completion factor (V), and I_L describes the light current (A) and is achieved by the following equation.

$$I_L = \frac{r}{r_{ref}} \times \left[I_L^{ref} - C_{I_L}^{ref} \times (T_c - T_c^{ref}) \right] \quad (18)$$

where r stands for solar radiation (W/m^2), r_{ref} is the reference solar radiation that is assumed 1000 (W/cm^2), I_L^{ref} describes the light currently at reference condition, $C_{I_L}^{ref}$ represents the temperature coefficient of the short-circuit current that is considered $A/25$ °C, and T_c and T_c^{ref} are the temperature of a PV cell (°C) and the reference temperature with value 25 °C, respectively.

The PV efficiency is highly affected by the temperature and the temperature is highly affected by different parameters such as solar radiation, output voltage, output current, and the ambient temperature. The relation between the PV module and the temperature is given in the following:

$$C_{PV} \times \frac{dT_c}{dt} = r_{PV} \times r - \frac{U \times I}{A_r} - C_{ht} (T_c - T_a) \quad (19)$$

where, C_{PV} represents the total heat capacity per unit area of the solar cell/module $J/(^{\circ}\text{C m}^2)$, r_{PV} describes the absorption rate for PV cells radiation, C_{ht} stands for the heat transfer coefficient [$\text{W}/(^{\circ}\text{C m}^2)$], T_a stands for the ambient temperature (°C). A_r describes the PV cell absorption area (m^2)

2.4. Model of wind energy conversion system

The generator of the wind turbine model is achieved based on the following formula (Chedid et al., 1998):

$$P_{WTG} = \begin{cases} 0 & v < v_{ci} \\ \frac{P_r \times (v^3 - v_{ci}^3)}{v_r^3 - v_{ci}^3} & v_{ci} \leq v \leq v_r \\ P_r & v_r \leq v \leq v_{co} \\ 0 & v > v_{co} \end{cases} \quad (20)$$

where, v_{ci} stands for the cut-in wind speed, v represents the local wind speed, v_{co} describes the cut-out wind speed, and v_r defines the rated wind speed for the wind turbine generator. Besides, the output power for the wind turbine is obtained by the following equation:

$$P_W = P_{WTG} \times A_W \times \eta_w \quad (21)$$

where, η_w defines the wind turbine generator efficiency where according to Betz's law, is no more than 16/27 (59.3%) of the kinetic energy in wind and A_W stands for the swept area of it (m^2).

2.5. Model of battery

In this part, a simple model of lead-acid has been employed. The model is considered by identical charge and discharge efficiencies about 0.88. To prevent the deep discharge, 20% capacity of the batteries does not take part in the charging/discharging processes. The left-over electricity of the battery when it is charged can be obtained as follows:

$$\begin{cases} P_{re} = P_{re} + 0.88 \times P_i^{ch} & P_i^{ch} \times 0.88 \geq P_C \\ P_{re} = P_C & P_i^{ch} \times 0.88 \leq P_C \end{cases} \quad (22)$$

And the left-over electricity of the battery when it is discharged is achieved as follows:

$$\begin{cases} P_{re} = P_{re} - 0.88 \times P_i^{ch} & \frac{P_{re} - P_i^{dis}}{0.88} \geq 0.20 \times P_C \\ P_{re} = P_C & \frac{P_{re} - P_i^{dis}}{0.88} \leq 0.20 \times P_C \end{cases} \quad (23)$$

where, P_{re} stands for the left-over electricity of the lead-acid battery, P_C describes the battery capacitance, P_i^{ch} and P_i^{dis} represent the electric energy charging/discharging into/from the battery.

3. Objective function for the cost

The total cost of the proposed hybrid PV/wind/PEMFC/battery is defined by an objective function as follows:

$$C_T = C_{PV} + C_{wind} + C_{PEMFC} + C_{battery} \quad (24)$$

Such that the cost of the PV conversion system, the storage battery, and a wind energy conversion system is obtained by the following:

3.1. The cost model of the PV conversion system

The total cost of photovoltaic conversion system is achieved as follows:

$$C_{PV} = \frac{I_{PV} - S_{PV} + Cm_{PV}}{N_p} \quad (25)$$

where, N_p describes the lifespan of the project, I_{PV} describes the initial cost of the PV energy conversion system as follows:

$$I_{PV} = \alpha_s \times A_s \quad (26)$$

The S_{PV} is the PV energy conversion system salvage value and is obtained as follows:

$$S_{PV} = S_s \times A_s \times \left(\frac{1 + \kappa}{1 + \gamma} \right)^{N_p} \quad (27)$$

The Cm_{PV} determines the maintenance cost of PV energy conversion system and is achieved as follows:

$$Cm_{PV} = \alpha_{cm_{PV}} \times A_s \times \sum_{i=1}^{N_p} \left(\frac{1 + \nu}{1 + \gamma} \right)^i \quad (28)$$

3.2. The cost model of the wind conversion system

The total cost of the wind energy conversion system is achieved by the following formulation:

$$C_{wind} = \frac{I_{wind} - S_{wind} + Cm_{wind}}{N_p} \quad (29)$$

where, N_p describes the lifespan of the project, I_{wind} describes the initial cost of the wind turbine generator as follows:

$$I_{PV} = \alpha_{wind} \times A_{wind} \quad (30)$$

The S_{wind} is the wind turbine generator system salvage value and is obtained as follows:

$$S_{wind} = S_{wind} \times A_{wind} \times \left(\frac{1 + \kappa}{1 + \gamma} \right)^{N_p} \quad (31)$$

The Cm_{wind} determines the maintenance cost of the wind turbine generator system and is obtained by the following formulation:

$$Cm_{wind} = \alpha_{cm_{wind}} \times A_{wind} \times \sum_{i=1}^{N_p} \left(\frac{1 + \nu}{1 + \gamma} \right)^i \quad (32)$$

3.3. The cost model of the battery

The total cost of the battery is considered as follows:

$$C_{battery} = \frac{I_{battery} + Cm_{battery}}{N_p} \quad (33)$$

where, $I_{battery}$ stands for the initial cost of the lead-acid battery and is achieved as follows:

$$I_{battery} = \alpha_{battery} \times P_C \times \sum_{i=1}^{N_b} \left(\frac{1 + \nu}{1 + \gamma} \right)^{\frac{i-1}{N_b}} \quad (34)$$

The $Cm_{battery}$ determines the maintenance cost of the lead-acid battery and is obtained as follows:

$$Cm_{battery} = \alpha_{cm_{battery}} \times P_C \times \sum_{i=1}^{N_p} \left(\frac{1 + \nu}{1 + \gamma} \right)^i \quad (35)$$

3.4. The cost model for the PEMFC

The capital cost of the PEM fuel cell based on (Tan et al., 2015) is as follows:

$$C_{PEMFC} = \left(C_{PEMFC}^{purchase} + C_{PEMFC}^{maintenance} + C_{PEMFC}^{amortization} \right) \times \left(\frac{N_{units}}{500000} \right)^{-0.362} \quad (36)$$

where,

$$C_{PEMFC}^{purchase} = 1.1 \times [0.027 \times A_{PEMFC} + 0.88] \times N_{PEMFC} + 0.24 \times N_{PEMFC} + 279.4 \quad (37)$$

Table 1

The details for parameters utilized in the hybrid system model.

Parameter	Value	Unit	Parameter	Value	Unit
N_p	20	year	ν	12	%
N_b	10	year	A_{PEMFC}	1.5	m^2
α_s	450	$\$/m^2$	S_s	45	$\$/m^2$
$\alpha_{cm_{PV}}$	4.3	$\$/m^2 \text{ year}$	γ	12	%
$\alpha_{cm_{wind}}$	2.5	$\$/m^2 \text{ year}$	N_{units}	1482	—
$\alpha_{cm_{battery}}$	100	$\$/m^2$	$f_{maintenance}$	0.06	—
α_{wind}	100	$\$/m^2$	$i_{capital}$	10	%
$\alpha_{cm_{battery}}$	10	$\$/m^2 \text{ year}$	S_{wind}	10	$\$/m^2$
κ	9	%			

$$C_{PEMFC}^{maintenance} = f_{maintenance} \times C_{PEMFC}^{purchase} \quad (38)$$

$$C_{PEMFC}^{amortization} = i_{capital} \times C_{PEMFC}^{purchase} \quad (39)$$

where, N_{units} represents the production volume of the PEMFC, $f_{maintenance}$ describes the maintenance factor of PEMFC, and $i_{capital}$ represents the capitalization ratio.

The details for the parameters are given in Table 1.

Fig. 4 shows the multi-objective optimization architecture for the proposed system.

4. Objective function for electricity efficiency

Another function that is utilized for the optimization of the hybrid system is to consider the electricity efficiency within 24 h as follows:

$$\eta = \frac{P_G}{P_{wind} + P_{PV}} \quad (40)$$

where, P_{PV} and P_{wind} describe the solar energy absorbed by the PV system and the wind energy absorbed by the wind energy conversion system, respectively and P_G stands for the electrical energy that is generated by the PV, wind energy conversion system, and the PEMFC stack and is obtained as follows:

$$P_G = P_L - P_{shrg} + P_{H_2}^{surplus} + (P_{re} - 0.20 \times P_c) \times 0.88 \quad (41)$$

where, P_L describes the 24-hours demand for total electric energy, $P_{H_2}^{surplus}$ defines the electric energy that is produced by the surplus hydrogen after 24 h's running, P_{shrg} stands for the mismatch between the electric energy and the users' demand, the term $(P_{re} - 0.20 \times P_c) \times 0.88$ determines the remained electricity energy in the battery storage after 24 h system running.

The input wind energy for energy conversion and the input solar energy for the PV conversion are given below:

$$P_{wind} = \int_0^{24} 0.5 \times \rho \times A_{wind} \times v^3 dt \quad (42)$$

$$P_{PV} = \int_0^{24} \phi \times A_{PV} \times N_s dt \quad (43)$$

where, N_s stands for the number of PV cells that are put in series and ρ describes the density of the local air.

5. Objective function for the energy supply reliability

This section explains the reliability of the energy supply as another part of the cost function for the hybrid system. this term can be determined based on the following equation:

$$R = \frac{P_L - P_{shrg}}{P_L} \quad (44)$$

Table 2

The optimization constraints for the hybrid system.

Parameter	Initial value	[Min. value, Max. value]	Unit
P_c	50	[50, 500]	—
N_s	200	[50, 200]	—
A_{wind}	50	[50, 500]	m^2
A_{PEMFC}	1000	[1000, 5000]	cm^2
N_{PEMFC}	100	[50, 500]	—

6. The total objective function

Based on the definitions in the previous sections, the study aims to optimize three different cost functions including the efficiency of the hybrid system, the capital cost, and the reliability of the energy supply. This makes the problem to be as a multi-objective optimization problem. Here, a developed model of a metaheuristic called Elephant Herding Optimization Algorithm (EHO) is used for this purpose. The optimization is done under some constraints. The total objective function in this study is illustrated below:

$$\text{Maximize}(\text{electricity efficiency } (\eta), \text{ power supply reliability } (R))$$

$$\text{Minimize}(\text{Capital cost } (C_T))$$

Subject to:

$$x_j \leq x_j \leq \bar{x}_j$$

where, x_j and \bar{x}_j stand for the lower and the upper limitations of the j th constraint. Five main parameters for the optimization of the above problem are given below (see Table 2).

7. Balanced elephant herding optimization algorithm

Evolutionary and metaheuristic algorithms (metaheuristics) are very powerful tools of artificial intelligence to solve optimization problems through intelligent methods and are nowadays widely used in several branches of science and engineering. These algorithms, which generally simulate the natural processes, are search methods that search for the best possible solution in the possible search space for an optimization problem. An important case that should be considered in metaheuristics is the dynamic balance between diversification and intensification. Diversification performs an extended searching in the search space and intensification indicates the solutions experienced during searching in the solution space. Considering the correct trade-off between these two strategies gives better solution space to the algorithms and decreases time-wasting. There are several models of metaheuristics such as Variance Reduction of Gaussian Distribution (VRGD) (Namadchian et al., 2016), Butterfly Optimization Algorithm (BOA) (Arora and Singh, 2019), Owl Search Algorithm (OSA) (Jain et al., 2018), Emperor Penguin Optimizer (EPO) (Dhiman and Kumar, 2018), Improved Cat Swarm Optimization (ICSO) algorithm (Kumar and Singh, 2018), World Cup Optimization (WCO) algorithm (Razmjoo et al., 2016), sunflower optimization (SFO) algorithm (Gomes et al., 2019), and Elephant herding optimization (EHO) (Wang et al., 2016).

Wang et al. proposed a new bio-inspired algorithm based on elephant herding behavior (Wang et al., 2016). Elephants are a kind of mammal animals that have big sizes. These animals have a long trunk that helps to breathe, lifting objects and drinking water. They also have strong legs to carry their weights. Naturally, in contrast, the male elephants that like to live alone upon growing up, female elephants have social behaviors and like to comprise the clans of females and the calves. They live in several clusters under the leadership of a matriarch that is usually the oldest one. However male elephants live independently from their family

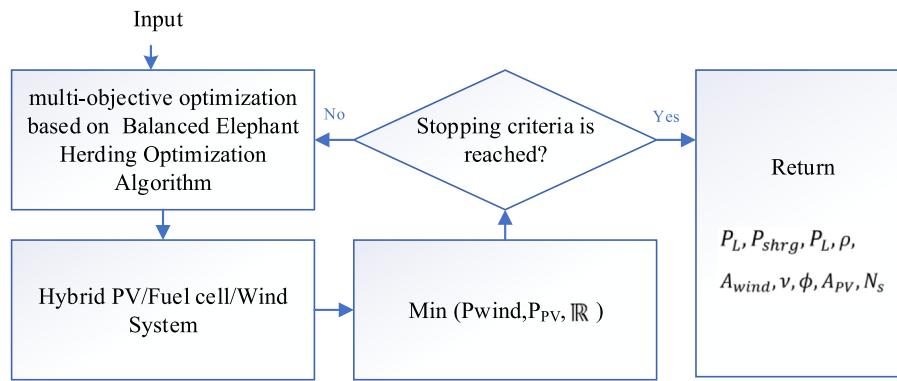


Fig. 4. The multi-objective optimization architecture for the proposed system.

group, they can connect with the family members over low-frequency vibrations. Each member of the elephant clans has high attention to the calves as the of a family group. This specific behavior has been a reason for proposing a new bio-inspired that is called Elephant Herding Optimization (EHO) Algorithm. The EHO Algorithm is based on the following characteristics:

7.1. Clan operator

As before mentioned, each clan has been led under the leadership of a matriarch. This case causes that matriarch ci affecting the next position of the elephants in clan ci . Therefore, the new position for the elephant j in clan ci ($x_{ci,j}^{new}$) is achieved as follows:

$$x_{ci,j}^{new} = x_{ci,j} + \alpha \times (x_{ci}^{best} - x_{ci,j}) \times r \quad (45)$$

where, $x_{ci,j}$ stands for the old position of elephant j in clan ci , x_{ci}^{best} describes matriarch ci that has the best solution in clan ci , α represents a scale factor to determine the impact of matriarch ci on $x_{ci,j}$ In the range $[0, 1]$ and $r \in [0, 1]$ is another random value.

And the updating formulation for the fittest elephant in each clan is achieved as follows:

$$x_{ci}^{new} = \beta \times x_{ci}^{center} \quad (46)$$

where β stands for a factor to define the effect of the x_{ci}^{center} on x_{ci}^{new} in the range $[0, 1]$.

In the above equation, $x_{ci,j}^{new}$ is obtained by considering the information from the elephants in clan ci and x_{ci}^{center} determines the center of clan ci . For the d th dimension, this term can be evaluated through D evaluations as follows:

$$x_{ci}^{center} = \frac{1}{n_{ci}} \sum_{j=1}^{n_{ci}} x_{ci,j}^d \quad (47)$$

where d determines the d th dimension in the range $[1, D]$, D stands for the total dimension, n_{ci} describes the total number of elephants in the clan ci , and $x_{ci,j}^d$ describes the d th case of the elephant candidate $x_{ci,j}$.

7.2. Separating operator

As before mentioned, male elephants live independently from the family when they have grown up. This feature is modeled in the EHO algorithm as a separating operator. This feature is modeled as follows:

$$x_{ci}^{worst} = \underline{x} + (1 + \bar{x} - \underline{x}) \times \delta \quad (48)$$

where, x_{ci}^{worst} describes the worst elephant individual in clan ci , $\delta \in [0, 1]$ is a random uniform distribution value, and \underline{x} and

\bar{x} represent the minimum and the maximum limitations of the elephant individual position, respectively.

More information about the EHO algorithm can be studied (Wang et al., 2016).

7.3. The balanced EHO algorithm

However, the EHO algorithm is a new and high-performance algorithm for optimization, it has also some issues that should be resolved. The main problem is the early convergence of the EHO algorithm. In this algorithm, the individuals gradually move in the search space near the best general optimum point and do not explore the rest of the space which is due to the inadequate balance mechanism between local and global search. This study proposes an improved version of the EHO algorithm for resolving this problem.

Here, the Lévy flight mechanism has been adopted for developing the EHO algorithm. This mechanism has a high capability to resolve premature convergence of the algorithm (Cao et al., 2019a,b; Fei et al., 2019) as a prominent shortcoming of the EHO. Lévy flight (LF) simulates a random walk mechanism for viable handling of the local search (Choi and Lee, 1998). This Lévy flight mechanism is modeled as follows:

$$Le(w) \approx w^{-1-\tau} \quad (49)$$

$$w = A \times |B|^{-1/\tau} \quad (50)$$

$$\sigma^2 = \left\{ \frac{\Gamma(1+\tau)}{\tau \Gamma((1+\tau)/2)} \frac{\sin(\pi \tau/2)}{2^{(1+\tau)/2}} \right\}^{\frac{2}{\tau}} \quad (51)$$

where, $\Gamma(.)$ is Gamma function, $0 < \tau \leq 2$, $A \sim N(0, \sigma^2)$, $B \sim N(0, \sigma^2)$, w stands for the step size, τ describes Lévy index, and $A/B \sim N(0, \sigma^2)$ point to the samples formed by a Gaussian distribution with a mean value of zero and variance of σ^2 . In this study, $\tau = 3/2$ (Li et al., 2018).

Based on the defined mechanism, the new updated equation for the clan and the separating operators are as follows:

$$x_{ci,j}^{new} = x_{ci,j} + \alpha \times (x_{ci}^{best} - x_{ci,j}) \times r \times Le(\delta) \quad (52)$$

$$x_{ci}^{worst} = \underline{x} + (1 + \bar{x} - \underline{x}) \times \delta \times Le(\delta) \quad (53)$$

where, $x_{ci,j}^{new}$ is the newly updated position for the elephant j in clan ci ($x_{ci,j}^{new}$), and x_{ci}^{worst} describes the new updated worst elephant individual in clan ci .

Besides, to guarantee of achieving the best solution candidates, fitter candidates have been kept:

$$x_{ci,j}^{new} = \begin{cases} x_{ci,j}^{new} & F(x_{ci,j}^{new}) > F(x_{ci,j}^{new}) \\ x_{ci,j}^{new} & \text{otherwise} \end{cases} \quad (54)$$

$$x_{ci}^{worst} = \begin{cases} x_{ci}^{worst} & F(x_{ci}^{worst}) > F(x_{ci}^{worst}) \\ x_{ci}^{worst} & \text{otherwise} \end{cases} \quad (55)$$

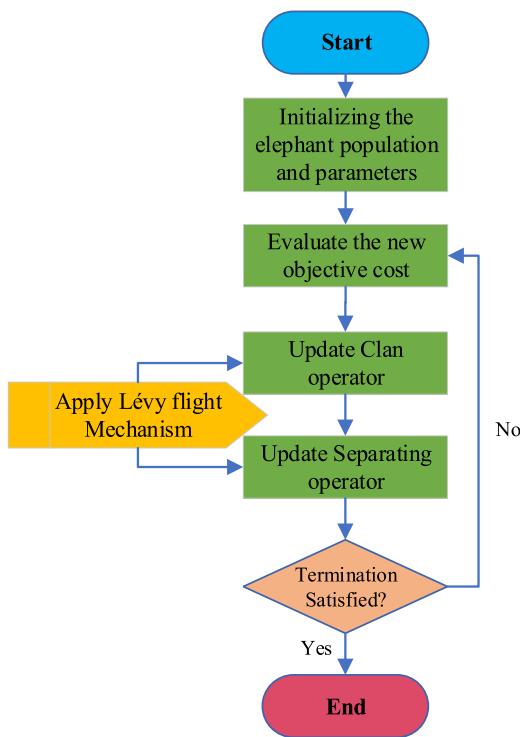


Fig. 5. The block diagram of the proposed BEHO.

Fig. 5 shows the block diagram of the presented BEHO.

8. Algorithm validation

In this section, to indicate the ability of the presented BEHO algorithm, it is validated by implementing it into some different functions. The results also compared with some different state of the art algorithms like genetic algorithm (GA) (Holland, 1992), particle swarm optimization algorithm (PSO) (Bansal, 2019), fluid search optimization algorithm (FSO) (Dong and Wang, 2018), world cup optimization algorithm (WCO) (Razmjooi et al., 2016), and the basic Elephant Herd Optimization (EHO) algorithm (Wang et al., 2016). The configuration of the selected laptop for simulation is Intel® Core™ i7-4720 HQ CPU@2.60 GHz with 16 GB RAM and the platform for the simulation is MATLAB R2017b. Table 3 indicates the utilized equations and their constraints for the validation with 30 dimensions.

After applying the utilized algorithms to the functions, the results for validation are achieved and provided in Table 4. This Table indicates the standard deviation value and the mean value of the compared methods by assuming 30-dimensions.

As can be seen, the best results are achieved by the EHO family for the adopted benchmark functions. The simulation for each algorithm has been run for 30 times to show its precision and standard deviation value. due to the minimum value of the BEHO algorithm, it can be considered as the highest accuracy algorithm among the compared methods. Besides, due to the low value of the standard deviation value, it has shown the highest precision among the others.

9. Simulation results

As before mentioned, the main purpose is to optimize a three-term multi-objective optimization including the energy supply reliability, the electricity efficiency, and the capital cost based on a newly introduced metaheuristic to achieve the best solution

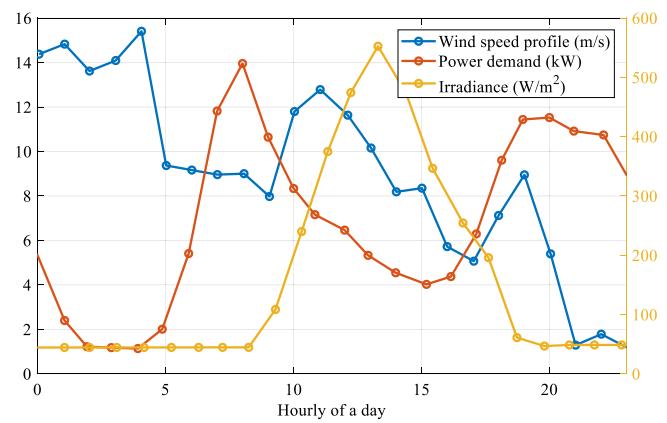


Fig. 6. Hourly profile of wind speed data, solar irradiance data, and the power demand data.

on a hybrid PV/wind/PEMFC/battery system. Fig. 6 Indicate the hourly profile of the solar irradiance data, wind speed data, and the power demand data, respectively that are used as the inputs for the case study. As can be seen, the wind speed during the 24 h starts with about 14.2 m/s in 12:00 and then after some descending oscillations, it reaches its lowest value about 1.1 m/s in 24:00. The results also show that from 8:00 to 13:00, an increasing irradiation occurs. In contrast, from 13:00 to about 18:00, the irradiance behaves as a downtrend process and after 18:00, this minimum value continues in about a side way value. Finally, by considering the power demand, it is clear the power demand in 12:00 is about 5.2 kW and this changes until 8:00 with maximum power demand. Another time of high power demand in the range 17:00 to 24.

For more clarifications about the Pareto solution set, the cost values of 300 optimal designs have been normalized in the range [0,1] and the results are shown in Table 5 and Fig. 7. From the results, it is clear that there are three scenarios for the system analysis: the minimum capital cost (S1), the maximum energy supply reliability (S2), and the maximum electricity efficiency (S3). Here, the S1 shows the high energy efficiency from 14.68% to 15.82%, with the corresponding cost from 2461\$/year to 3083 \$/year with energy supply reliability from 77.20% to 80.47%. The S3 shows the low capital cost from 2834 \$/year to 2934 \$/year and the electricity efficiency in the range 17.53% and 18.74% along with energy supply reliability from 76.24% to 76.89%. Finally, S2 gives a high energy supply reliability in the range 85.36% and 87.82% with the capital cost from 2846 \$/year to 3373 \$/year and with the electricity efficiency in the range 8.61% and 11.75%.

Therefore, if the main objective is to focus on the lower capital cost of the hybrid system, S1 (with sacrificing the energy supply reliability), is the best selection, if the main objective is to emphasize on the higher energy supply reliability, S2 gives the best selection (of course by losing the ability for the other two aspects, and if the main objective is to obtain higher electricity efficiency of the hybrid system with losing the other two aspects, S3 is the best selection.

For more clarification of the results, the study uses the approximated Pareto front. Generally, to obtain the desired performance, the decision variables values can be found by the decision makers. In other words, these results help the decision variables to consider what should be sacrificed to obtain better efficiency for the other objective function. Besides, after determining the design variables, the dynamic response of the units can be observed by the provided models according to the weather and load conditions. By this way, the design makers can recognize how to choose the size of units in the hybrid system for decreasing the

Table 3
The utilized benchmarks for efficiency analysis.

Function	Equation	Constraint
Ackley	$f_1(x) = -20 \exp \left(-0.2 \sqrt{\frac{1}{D} \sum_{i=1}^D x_i^2} \right) - \exp \left(\frac{1}{D} \sum_{i=1}^D \cos(2\pi x_i) \right) + 20 + e$	[-10, 10]
Rastrigin	$f_2(x) = 10D + \sum_{i=1}^D (x_i^2 - 10 \cos(2\pi x_i))$	[-512, 512]
Rosenbrock	$f_3(x) = \sum_{i=1}^{D-1} (100(x_i^2 - x_{i+1}) + (x_i - 1)^2)$	[-2.045, 2.045]
Sphere	$f_4(x) = \sum_{i=1}^D x_i^2$	[-512, 512]

Table 4
The validation results of the compared methods.

Benchmark	BEHO	EHO (Wang et al., 2016)	GA (Holland, 1992)	PSO (Bansal, 2019)	WCO (Razmjoo et al., 2016)	FSO (Dong and Wang, 2018)
f_1	mean	0.00	9.38e-18	4.18e-2	7.85	4.28e-3
	std	0.00	0.00	3.53e-2	2.16	2.14e-3
f_2	mean	0.00	1.98	70.61	74.24	2.19
	std	0.00	1.58	1.66	8.96	4.35
f_3	mean	5.48	5.84	35.41	200.1	13.16
	std	3.61	1.32	27.15	59.00	4.62
f_4	mean	0.00	5.28e-14	1.62e-4	7.59e-4	5.27e-9
	std	0.00	2.37e-18	2.57e-5	4.93e-4	2.74e-9

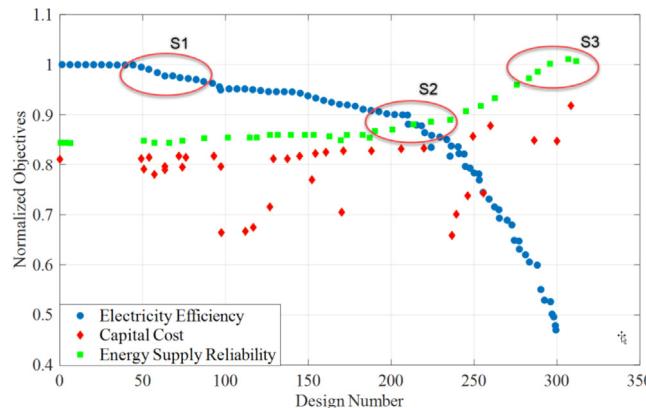


Fig. 7. Normalized objectives for 300 designs of the proposed hybrid system.

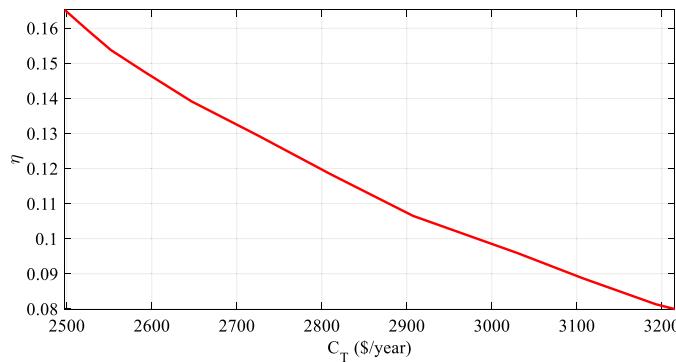


Fig. 8. Pareto front of the electricity efficiency and the energy supply reliability.

renewable energy fluctuation by the help of Pareto front (see Fig. 8).

Therefore, based on the above results and the Pareto front, the decision-makers can provide the best selection based on their positions.

Table 5
The cost function values for different scenarios.

Cost function	S1	S2	S3
η (%)	14.68–15.82	8.61–11.75	17.53–18.74
\mathbb{R} (%)	77.20–80.47	85.36–87.82	76.24–76.89
C_T (\$/year)	2461–3083	2846–3373	2834–2934

10. Conclusions

This study proposed a multi-objective optimization structure for a hybrid PV/Wind/PEMFC/Battery system. The optimization configuration included three parts of cost minimization, energy supply reliability maximization, and electricity efficiency maximization. The optimization process was performed using a new balanced model of the Elephant Herding Optimization (BEHO) Algorithm. The purpose of the study was to determine the Pareto surface of the problem to make the decision operation easy for decision-makers.

The proposed method analyzed three different scenarios including minimum capital cost (S1), maximum energy supply reliability (S2), and maximum electricity efficiency (S3). The final results showed that the only case for selecting the best configuration is to check the Pareto solution set. In addition to the parameters that are considered for the optimization in this work, there are some other parameters that can effect on the system, for example, PEMFC area and number of PEMFC cells that give an inspiration to work on them in the future work.

CRedit authorship contribution statement

Yan Cao: Conceptualization, Data curation, Writing - original draft, Writing - review & editing. **Hui Yao:** Conceptualization, Data curation, Writing - original draft, Writing - review & editing. **Zhijie Wang:** Conceptualization, Data curation, Writing - original draft, Writing - review & editing. **Kittisak Jermitsuparsert:** Conceptualization, Data curation, Writing - original draft, Writing - review & editing. **Nasser Yousefi:** Conceptualization, Data curation, Writing - original draft, Writing - review & editing.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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